# Practical Application of Functional and Relational Methods for the Specification and Verification of Safety Critical Software

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## **Outline**

- Motivation
- Mathematical Preliminaries
- Functional 4-Variable Model & its decomposition
- Example of Functional Limitations
- Relational 8-Variable Model
- Conclusions & Further Research

## Motivation: Reactor Shutdown System (SDS)

#### What is an SDS?

- watchdog system that monitors system parameters
- shuts down (trips) reactor if it observes "bad" behavior
- process control is performed a separate Digital Control computer (DCC) not as critical

#### Why use formal verification?

- Spurious trips cost \$\$\$
- Difficult to make modifications & even more difficult to get regulatory approval for changes
- Minor changes result in another extensive (& expensive) round of testing & review
- Testing can't cover all possible cases
- Too much detail for person to catch everything by review

# Motivation: (cont)

The CANDU Computer Systems Engineering Centre of Excellence Standard for Software Engineering of Safety Critical Software (Joannou et al.) first fundamental principle states:

"The required behavior of the software shall be documented using mathematical functions in a notation which has well defined syntax and semantics."

Why use functions?

**Determinism:** Want unambiguous description of safety critical behavior

Clarity: Easier to understand functional requirements

**Preference:** Engineers prefer to specify precise behavior and appeal to tolerances when necessary

**Sufficient:** Functional methods often sufficient - Work "most of the time" & are easily automated

# Motivation (cont)

Verification uses tabular methods, custom tools and SRI's PVS automated proof assistant to handle typechecking and proof details.

Over 100 verification "blocks" in system. Each block typically has multiple inputs.

#### Goals:

- Make formal methods practical: Minimize effort required to perform systematic design verification.
- Address functional limitations by formalizing tolerance arguments.

#### How?

- Use of simple algebraic properties can reduce effort required for formal verification.
- Introduce 8-variable model.

#### **Preliminaries**

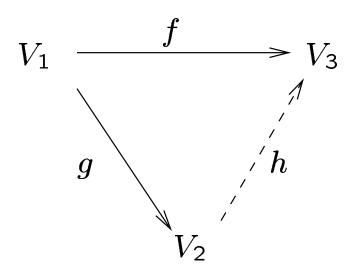
Let  $g: V_1 \to V_2$  and  $h: V_2 \to V_3$ , then  $h \circ g$  denotes functional composition.

Let  $G \subseteq V_1 \times V_2$  and  $H \subset V_2 \times V_3$ , then  $G \bullet H$  denotes relational composition.

Given equivalence relations  $E_1, E_2 \subseteq V \times V$ , define partial order  $E_1 \leq E_2$  iff  $(\forall v, v' : V)((v, v') \in E_1 \Rightarrow (v, v') \in E_2)$ .

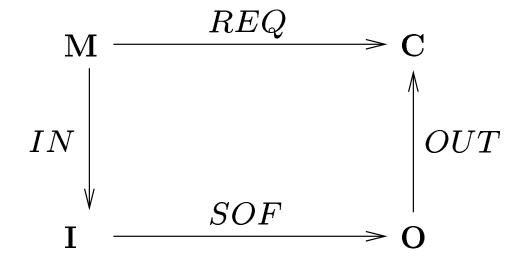
Given  $f: V_1 \to V_3$ , define  $\ker(f)$ , the *equivalence kernel of* f to be the equivalence relation given by:  $(v_1, v_1') \in \ker(f)$  iff  $f(v_1) = f(v_1')$ .

#### Claim:



 $(\exists h: V_2 \to V_3)f = h \circ g \text{ iff } \ker(g) \leq \ker(f)$ 

## 4-Variable Model (Parnas & Madey)



 $\mathbf M\,$  - Monitored Variables statespace

C - Controlled Variables statespace

I - Input Variables statespace

O - Output Variables statespace

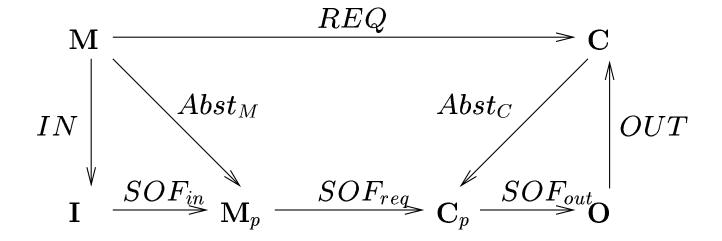
M, C, I, O are time series vectors and REQ, SOF, IN, OUT are relations.

We use a special case where all relations are functional resulting in proof obligation:

$$REQ = OUT \circ SOF \circ IN \tag{1}$$

Here REQ and SOF are the one step transition functions of the requirements and design respectively.

# "Vertical" Decomposition



$$Abst_C \circ REQ = SOF_{req} \circ Abst_M \tag{2}$$

$$Abst_M = SOF_{in} \circ IN \tag{3}$$

$$id_{\mathbf{C}} = OUT \circ SOF_{out} \circ Abst_{C}$$
 (4)

 $\mathbf{M}_p$  and  $\mathbf{C}_p$  are the *pseudo-monitored* and *pseudo-controlled* "variables" corresponding to software's internal representation of monitored and controlled quantities

- (2) represents main verification block
- (3) and (4) represent hardware hiding modules

# Hardware Hiding Example

E.g. temperature of the primary heat transport system which belongs to  $\mathbf{M}$  might have a value of 500.3 Kelvin.

A/D converters map this via IN to a value of 3.4 volts in a parameter of  $\mathbf{I}$ .

A hardware hiding module might then process this input corresponding to map  $SOF_{in}$ , producing a value of 500 Kelvin in the appropriate temperature variable of the software state space  $\mathbf{M}_p$ .

# "Vertical" Decomposition (cont)

More "vertical" decomposition obtained by isolating outputs. In effect,

- i) projecting C onto single output
- ii) restricting REQ to relevant subset of M

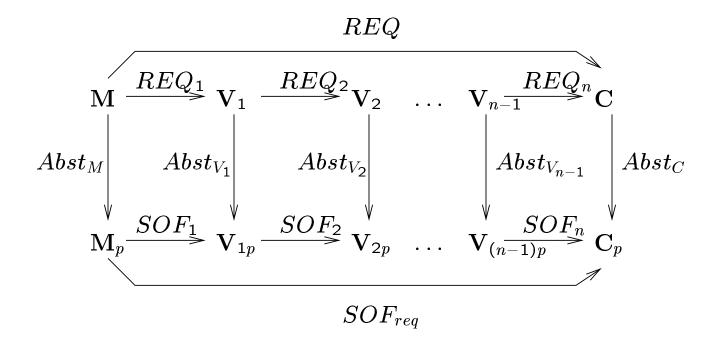
Note "wrong way"  $Abst_C$  arrow - used to reduce number of required abstraction functions

Can reduce by up to 1/2 number of abstraction functions required.

Proof obligation (4) precludes possibility of trivial implementations

Invertibility of OUT not possible in all situations but applicable to majority of safety critical requirements

# "Horizontal" Decomposition



Main block comparison can be sequentially decomposed into sequence of simpler obligations of the form:

$$SOF_i \circ Abst_{V_{i-1}} = Abst_{V_i} \circ REQ_i$$
 (5)

Cost of decomposition? Verifier must provide cross reference in form of  $Abst_{V_i}: V_i \rightarrow V_{ip}$ .

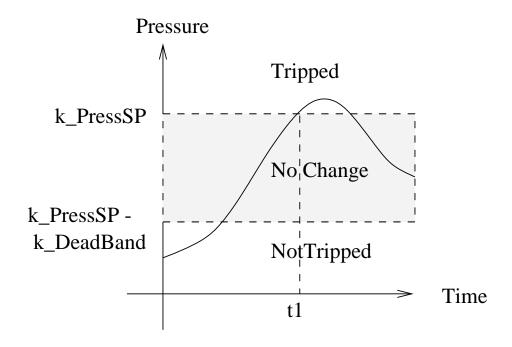
Now we see benefit of "wrong way" arrow: Same  $Abst_{V_i}$  can be used on output then input of successive blocks.

**Note:** Only need to check invertibility of  $Abst_C$  to satisfy (4).

## **Pressure Sensor Trip Example**

Idea: when pressure exceeds setpoint, reactor is "tripped" (shutdown).

Deadband where no change occurs is used to eliminate sensor "chatter".



Required behavior is specified by function f\_PressTrip and implemented by PTRIP.

In the function definitions, f\_PressTripS1 and PREV are corresponding state variables.

# Pressure Sensor Trip Example (cont)

Abstraction functions posreal2AI and Trip2bool map abstract datatypes to concrete implementations.

posreal2AI models the A/D conversion by taking integer part of sensor values in [0, 5000] mV range.

Return type, AI, consists of integers between 0 and 5000.

Resulting block comparison commutative diagram is:

$$\begin{array}{c|c} \mathsf{posreal} \times \mathsf{Trip} & \frac{f\_PressTrip}{} > \mathsf{Trip} \\ posreal2AI \times & Trip2bool & Trip2Bool \\ \mathsf{AI} \times \mathsf{bool} & \frac{PTRIP}{} > \mathsf{bool} \end{array}$$

# **PVS** for Pressure Sensor Trip

sentrip: theory

begin

 $k_PressSP: int = 2450$  $k_DeadBand: int = 50$ 

KDB: int =  $k_DeadBand$ KPSP: int =  $k_PressSP$ 

Trip: type =  $\{Tripped, NotTripped\}$ 

AI: type = subrange(0,5000)

Pressure $\leq$ k_PressSP $-$ k_DeadBand	NotTripped
k_PressSP — k_DeadBand < Pressure	f_PressTripS1
∧ Pressure < k_PressSP	
Pressure $\geq k_PressSP$	Tripped

endtable

PTRIP(PRES: AI, PREV: bool): bool = table

, , , , , , , , , , , , , , , , , , , ,	
PRES ≤ KPSP - KDB	FALSE
KPSP - KDB < PRES ∧ PRES < KPSP	PREV
$PRES \ge KPSP$	TRUE

endtable

Trip2bool(TripVal : Trip) : bool = table

TripVal = Tripped	TRUE
TripVal = NotTripped	FALSE

endtable

# PVS for Pressure Sensor Trip (cont)

posreal2AI(x : posreal) : AI = table

$x \leq 0$	0
$0 < x \wedge x < 5000$	floor(x)
$x \ge 5000$	5000

endtable

Sentrip1: theorem

(∀ (Pressure : posreal, f\_PressTripS1 : Trip) :
 Trip2bool(f\_PressTrip(Pressure, f\_PressTripS1)) =
 PTRIP(posreal2AI(Pressure), Trip2bool(f\_PressTripS1)))

end sentrip

Attempting block comparison theorem Sentrip1 reduces to proving for all inputs:

 $\neg$ (f\_PressTripS1 = Tripped $\land$  2400 < Pressure < 2450  $\land$  floor(Pressure)  $\le$  2400)

Counter examples result when Pressure  $\in$  (2400, 2401) and f\_PressTripS1 = Tripped.

In fact there does not exist a design that can satisfy requirement f\_PressTrip since

 $ker(posreal2AI \times Trip2bool) \not\leq ker(f\_PressTrip)$ 

## Pressure Sensor Trip Example (cont)

While it is possible to "fix" specification so that it is implementable by changing inequalities as follows:

Pressure < k_PressSP — k_DeadBand	
$k_PressSP - k_DeadBand \leq Pressure$	f_PressTripS1
∧ Pressure < k_PressSP	
Pressure $\geq k_PressSP$	Tripped

endtable

in practice this difference is a mathematical irrelevancy since A/D converters have  $\pm 5 \text{mV}$  accuracy.

#### Want to:

- maintain functional requirements specification and design description, and
- use formal mathematical proofs incorporating tolerances when necessary without an excessive increase in proof complexity and documentation.

#### 8-Variable Model

REQ and SOF still functions MTOL, CTOL are Input/Output tolerance relations

$$REQUIREMENTS = MTOL \bullet REQ \bullet CTOL$$

$$DESIGN = IN \bullet SOF \bullet OUT$$

Design verification amounts to showing:

$$DESIGN \subseteq REQUIREMENTS$$
, and (6)  
 $DESIGN$  is total (7)

## 8-Variable Model (cont)

In the standard 4-variable model this is modeled by the relation  $NAT \subseteq \mathbf{M} \times \mathbf{C}$ . In the case of the proposed 8-variable model we could have  $NAT \subseteq \mathbf{BM} \times \mathbf{BC}$ . In this case (7) could be replaced by the requirement:

$$dom(NAT) \subseteq dom(DESIGN)$$
 (8)

#### Sensor Trip Revisited

Revised block comparison theorem is easily proved:

```
Sentrip1: theorem (\forall (Pressure : posreal, f\_PressTripS1 : Trip) (\exists (Pressure2 : {(x : posreal)|Pressure - 5 \le x \le Pressure + 5}) : Trip2bool(f\_PressTrip(Pressure2, f\_PressTripS1)) = PTRIP(posreal2AI(Pressure), Trip2bool(f\_PressTripS1))))
```

#### **Conclusions**

- Tool supported functional 4-variable model using tabular methods has been successfully applied to Darlington SDS
- Decomposition of 4-var model reduces effort required to perform and document verification process
- Simple algebraic "tricks" can make formal methods more practical for industry
- 8-variable Relational model preserves functional specification of requirements and implementation & addresses functional limitations

## **Future Work**

- automating verification and re-verification tasks
- modeling & verification of concurrent realtime properties with tolerances
- equivalence verification, model-checking & model reduction